

# **Estimating injectivity for saline** aquifers – The UKSAP method

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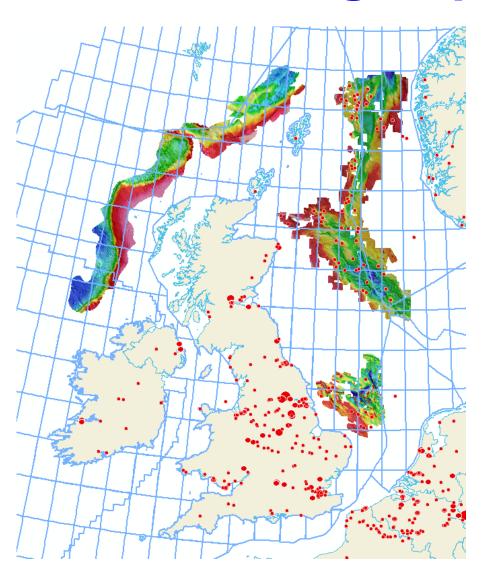




#### **Outline**

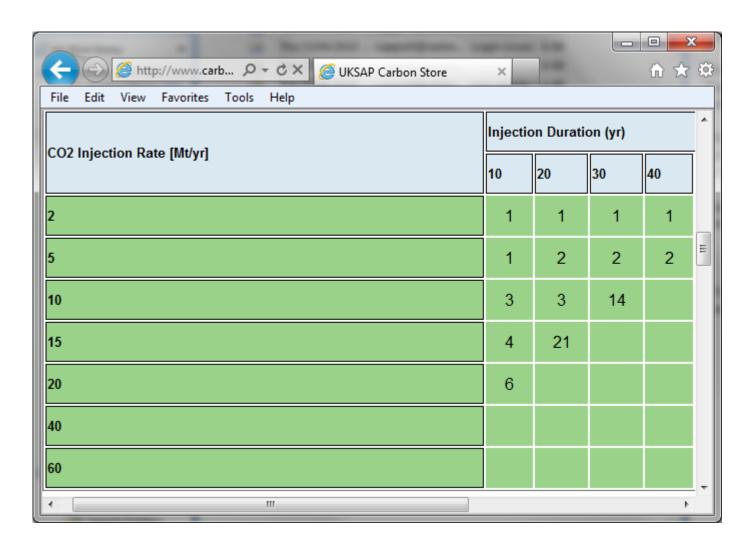
- UKSAP injectivity method.
- Preliminary results and economic implications.
- Simplifying assumptions.
- Role of partial miscibility.
- Sensitivity to uncertainty concerning relative permeability data.
- Role of heterogeneity.
- Pressure data from Snohvit.

# **UK Storage Appraisal Project**



Depth to top of reservoir [m]				
Area of formation [km <sup>2</sup> ]				
Av Gross Thickness [m]				
Av Vertical NTG [frac]				
Av Porosity [frac]				
Storage Formation Permeability [mD]				
Temperature [°C]				
Salinity [kg/l]				
Porosity (%)				
Rock compressibility [MPa <sup>-1</sup> ]				
Residual water saturation [-]				
CO <sub>2</sub> end-point relative permeability [-]				
Formation fracture pressure [MPa]				
Virgin formation pressure [MPa]				

#### **Number of wells matrix**

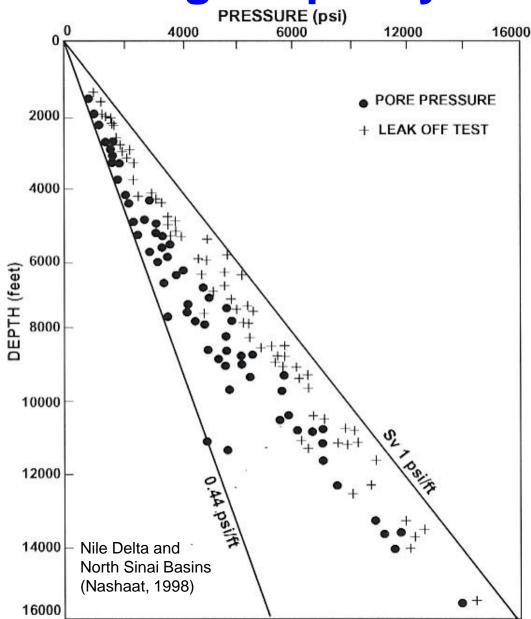


#### Pressure limited storage capacity

As CO<sub>2</sub> is injected, pressure increases.

It is necessary to avoid exceeding the fracture pressure of the cap-rock.

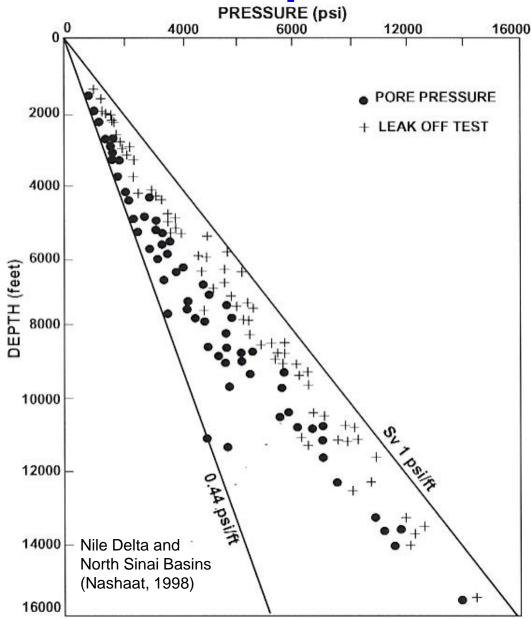
The amount of CO<sub>2</sub> that can be stored is often pressure limited.



#### **UKSAP** maximum allowable pressure

#### The minimum of:

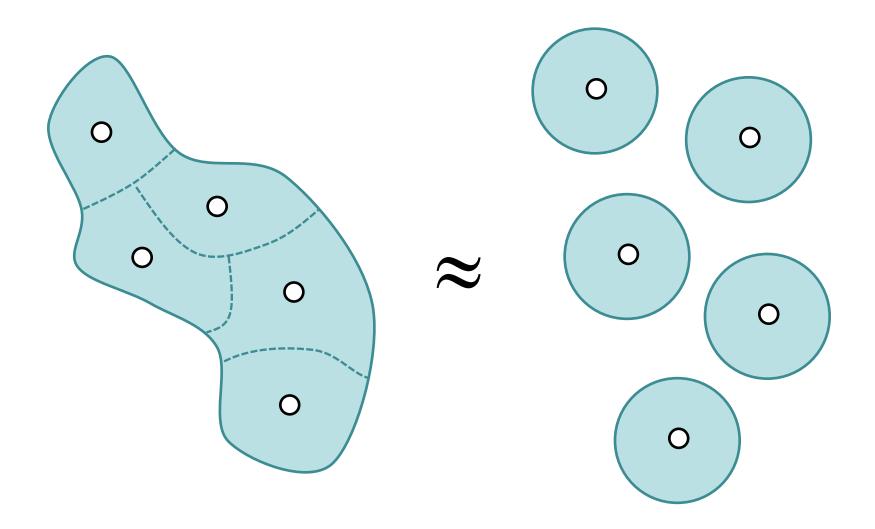
- 1. 90% of the fracture pressure;
- 90% of the lithostatic pressure (the overburden);
- 3. 100% estimated maximum downhole pressure that can be sustained by a surface pressure of 25 MPa (surface pressure + gravity head frictional loss).



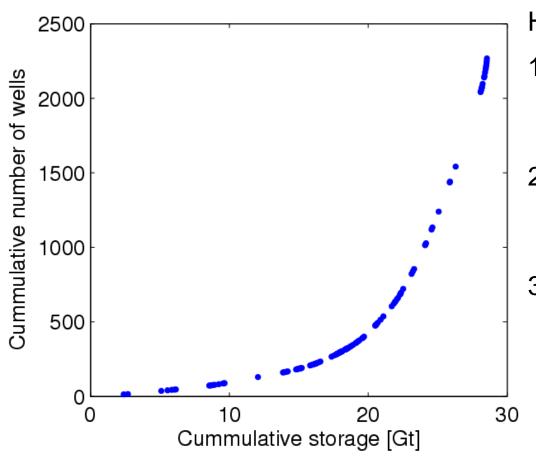
#### Workflow

- 1. Calculate maximum pressure buildup in the injection well due to constant injection of CO<sub>2</sub>.
- 2. If the pressure buildup > maximum allowable pressure the domain is split up to accommodate an additional injection well.
- 3. Injection rate is then distributed between wells and maximum pressure buildup is reassessed.
- 4. Number of wells sequentially increased until estimated maximum pressure buildup < maximum allowable pressure.

# Multiple well studies



# Preliminary results from 200 closed saline aquifers

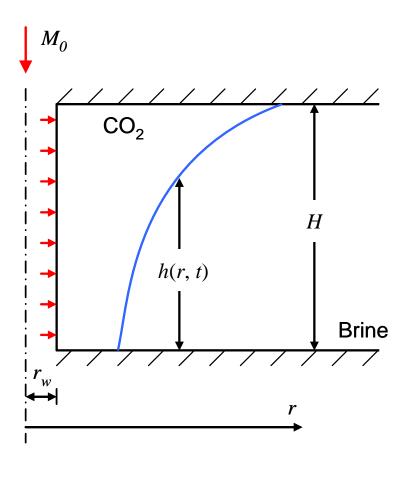


How do you want to report it?

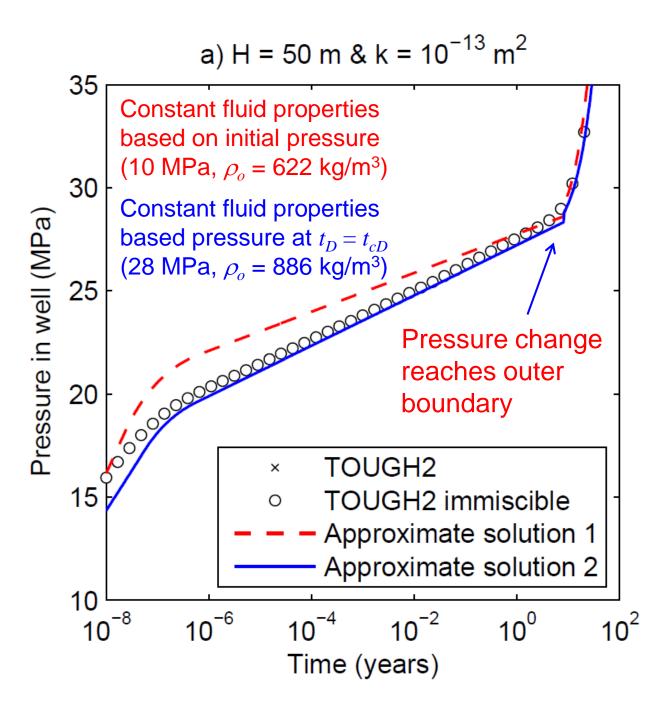
- 1) At least 2500 wells needed to store less than 30 Gt of CO<sub>2</sub>.
- 2) 1030 wells required to store total UK emissions for 40 years (~24 Gt).
- 3) Cost of drilling wells for storing 40 years of UK emissions £0.43 / t CO<sub>2</sub> (assuming 10 million £ per well).

Results are based on one deterministic realisation using maximum likelihood parameters.

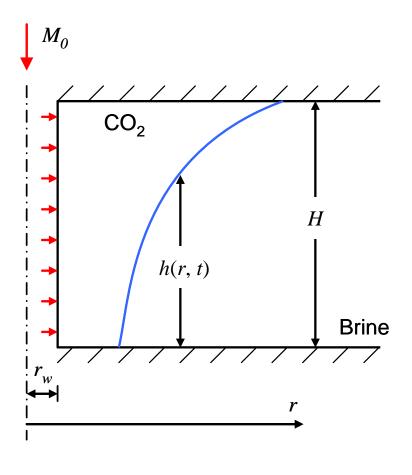
#### **Simplifying assumptions**



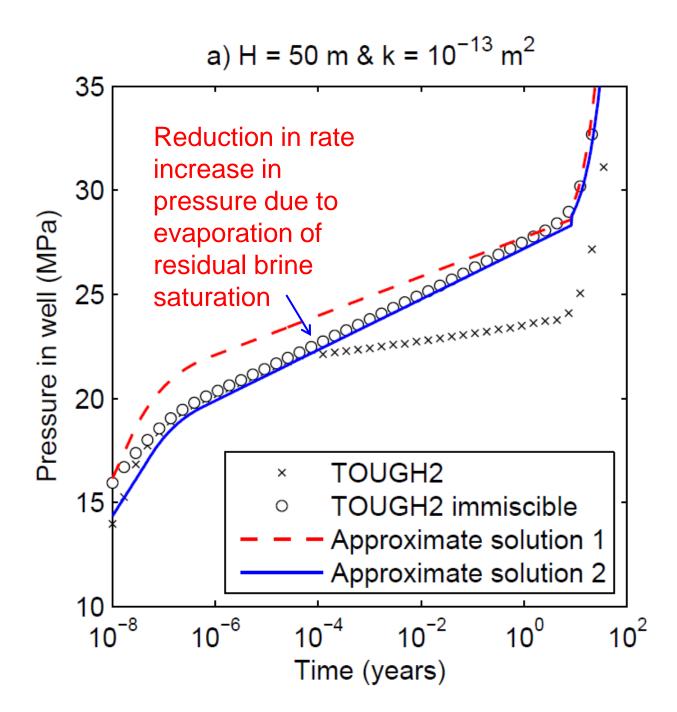
- 1) Vertical pressure equilibrium.
- 2) Negligible capillary pressure.
- 3) Constant fluid properties.
- 4) Immiscible flow (no brine evaporation and no CO<sub>2</sub> dissolution).
- 5) Linear relative permeability.
- 6) Homogenous and isotropic formation.



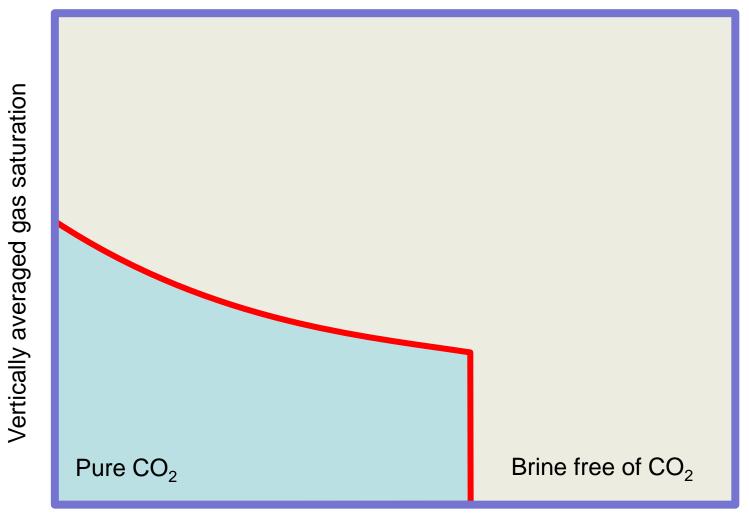
## **Simplifying assumptions**



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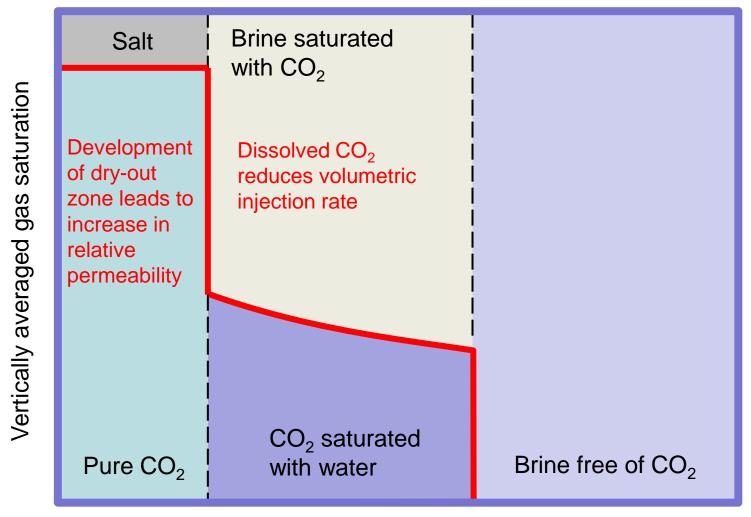
#### Fully immiscible displacement



Radial distance from injection well

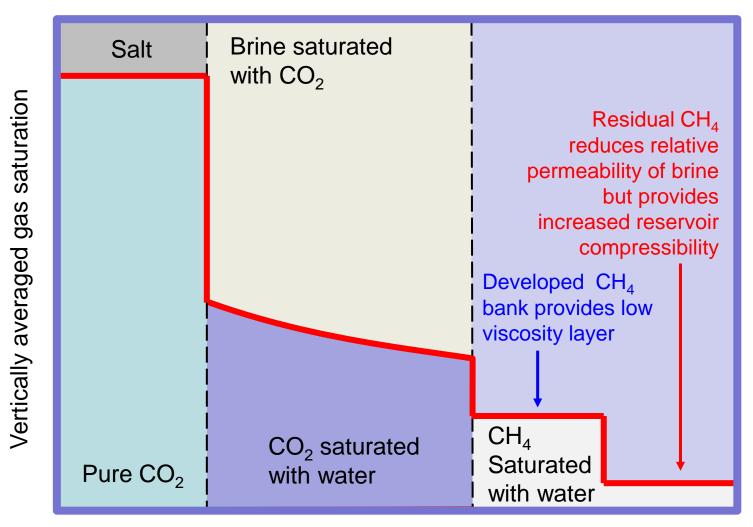
#### Partially miscible displacement

Precipitation of salt reduces relative permeability



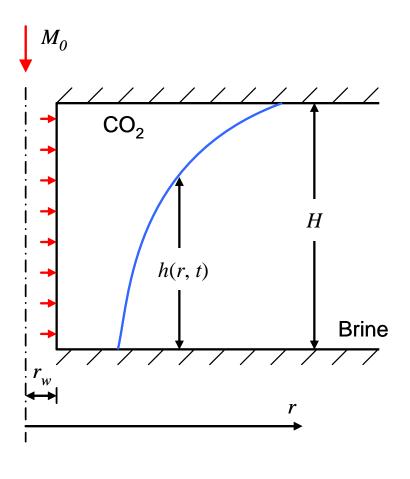
Radial distance from injection well

#### Residual and/or dissolved CH<sub>4</sub>



Radial distance from injection well

## **Simplifying assumptions**



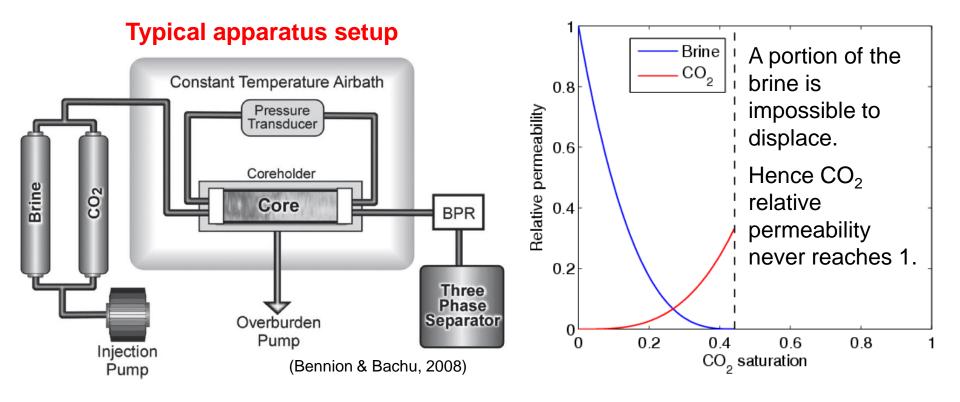
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## What is relative permeability?

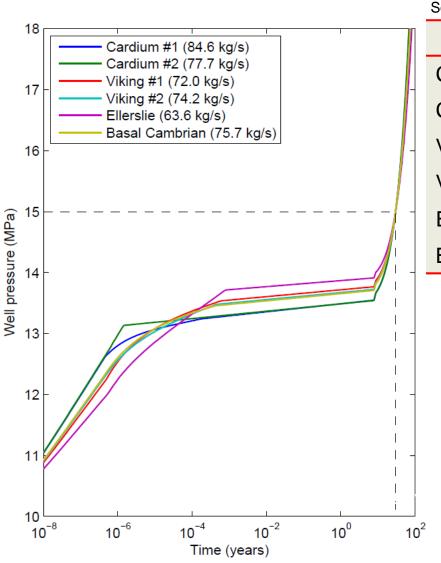
When a porous medium is partially saturated with different fluid phases only a fraction of the intrinsic permeability is available to each fluid.

Relative permeability is this fraction.

Normally obtained from core-flood experiments.

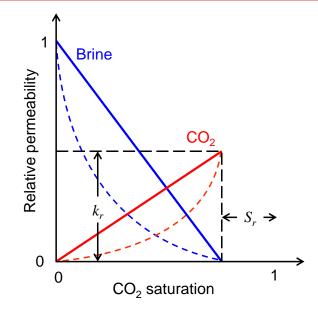


#### Bennion and Bachu's six sandstone cores

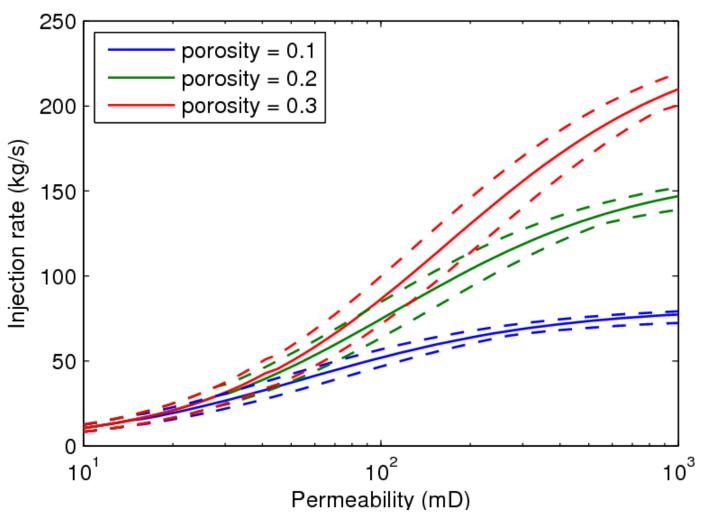


Some data for sandstones (after Bennion and Bachu, 2009)

	$k_r$	$S_r$	Brine exp	CO <sub>2</sub> exp
C1	0.53	0.20	1.3	1.7
C2	0.13	0.43	1.2	1.3
V1	0.33	0.56	2.9	3.2
V2	0.26	0.42	1.7	2.8
E	0.12	0.66	2.1	2.2
ВС	0.54	0.29	1.8	5.0



#### Sensitivity to uncertainty in rel-perm data



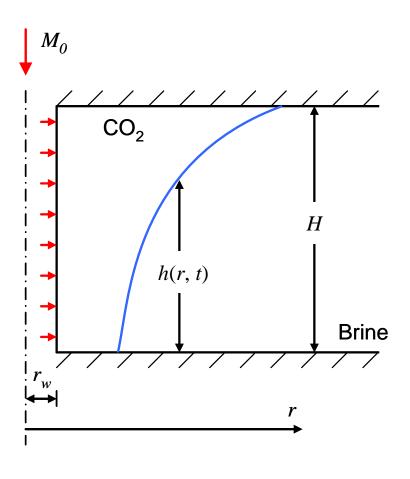
Pressure change = 5 MPa

Temperature = 40°

Formation thickness = 200 m

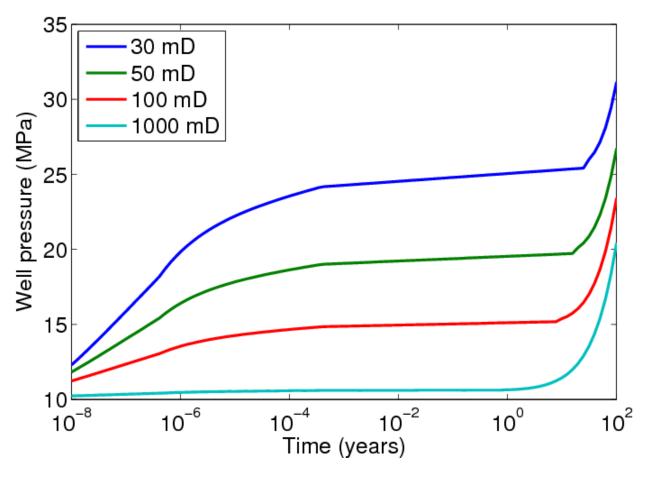
Formation area =  $1250 \text{ km}^2$ 

#### **Simplifying assumptions**



- 1) Vertical pressure equilibrium.
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## Effect of permeability on pressure



Injection rate = 3 Mt/yr

Formation thickness = 200 m

Porosity = 20%

Formation area =  $1250 \text{ km}^2$ 

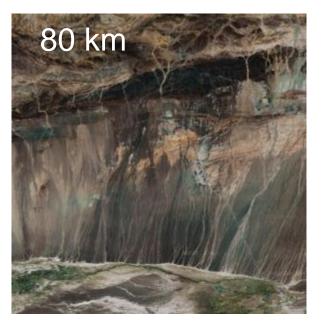
#### Stochastic simulation of channels

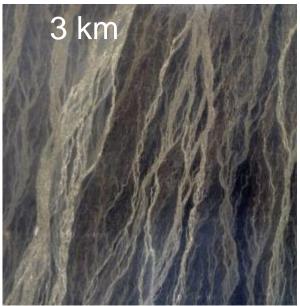
#### Bunter sandstone outcrop

- Fluvial channels deposited in an arid environment of alluvial fans.
- Similar to Tarim Basin, China.



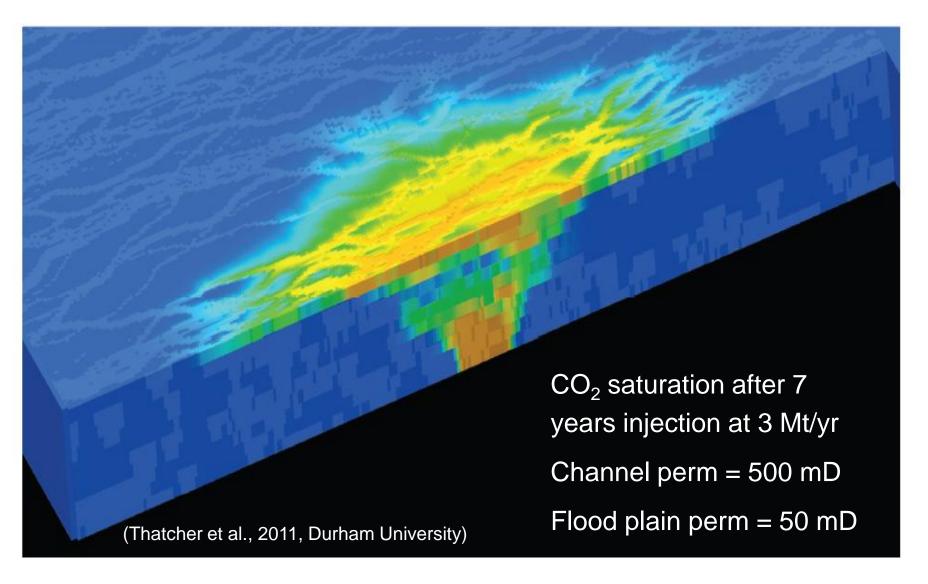
Channel widths 10s to 100s meters. Need grid cells around 5 x 5 m to resolve channel structures.

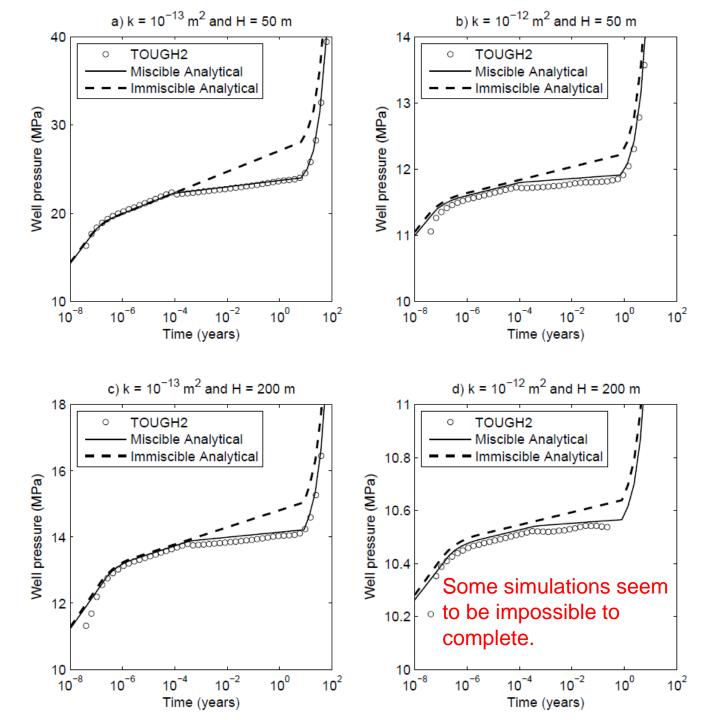






# Influence of permeability



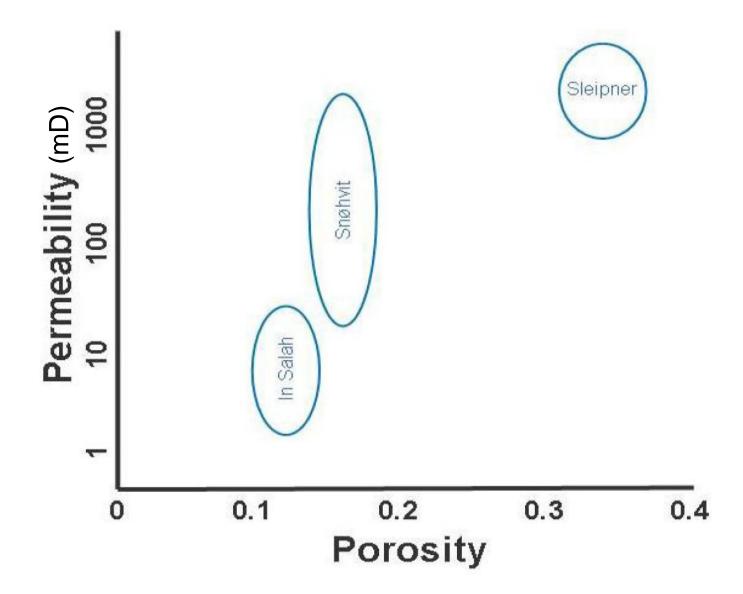


## **Snohvit Project, North Sea**

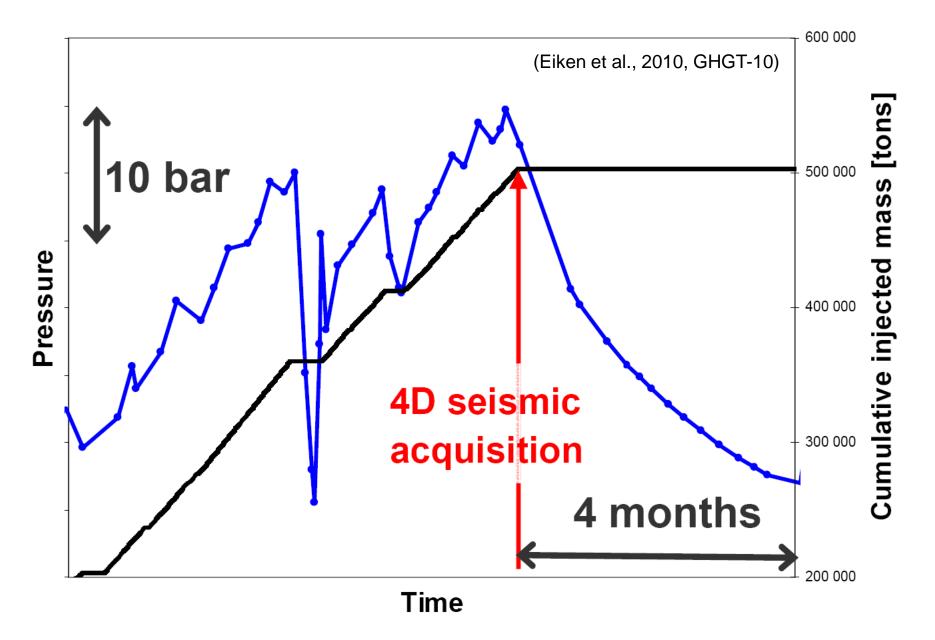
- Snøhvit (Snow White) is an LNG project, in the Barents Sea offshore Norway
- CO<sub>2</sub> is captured onshore and transported in a 153km subsea pipeline to a subsea template.
- The CO<sub>2</sub> is injected at a depth of 2600m into the Tubåen formation (below the gas reservoir).
- Injection of CO<sub>2</sub> started in 2008, and so far 1.0 Mt have been stored.



## Permeability of demonstration projects



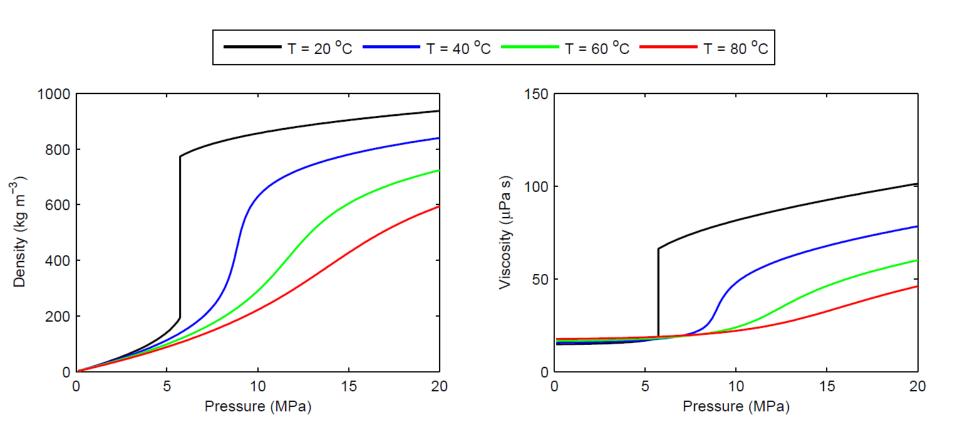
#### **Pressure record from Snohvit**



## **Summary and conclusions**

- Storing UK emissions may involve drilling 1000s of wells but cost of drilling is likely to be trivial compared to capture costs.
- Salt precipitation around injection wells is likely to occur but is likely to be compensated for by evaporation of residual brine.
- There is major uncertainty concerning relative permeability of CO<sub>2</sub> brine mixtures. But associated uncertainty appears less significant for injectivity in the context of permeability and porosity uncertainty.
- Fine-scale heterogeneity (10 m scale) is likely to be important, but investigating this further has been challenging using available simulation methods.

# Fluid properties of CO<sub>2</sub>



# Typical vertical profile

